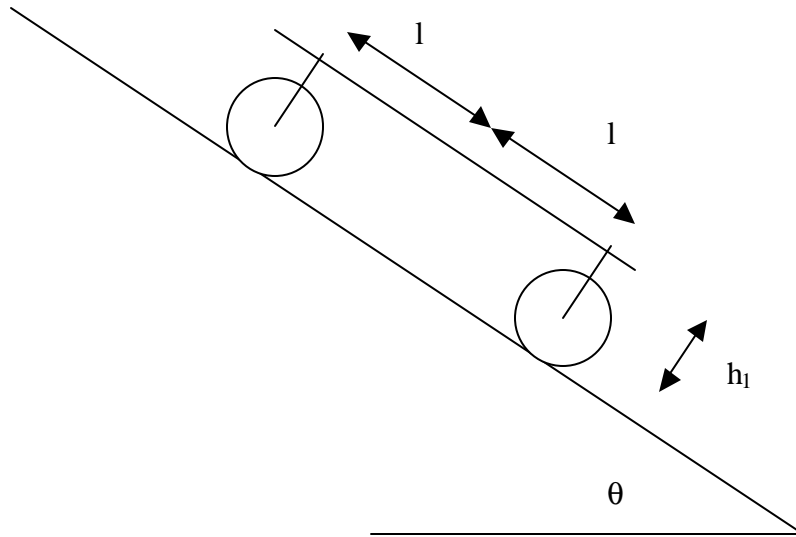


SOLUTION T3 :. A Heavy Vehicle Moving on An Inclined Road



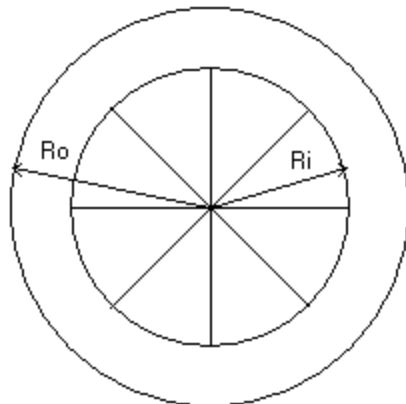
To simplify the model we use the above figure with $h_1 = h + 0.5 t$
 $R_o = R$

1. Calculation of the moment inertia of the cylinder

$$R_i = 0.8 R_o$$

Mass of cylinder part : $m_{\text{cylinder}} = 0.8 M$

Mass of each rod : $m_{\text{rod}} = 0.025 M$



$$I = \oint_{\text{wholepart}} r^2 dm = \oint_{\text{cyl.shell}} r^2 dm + \oint_{\text{rod1}} r^2 dm + \dots + \oint_{\text{rodn}} r^2 dm \quad 0.4 \text{ pts}$$

$$\begin{aligned} \oint_{\text{cyl.shell}} r^2 dm &= 2\psi \int_{R_i}^{R_o} r^3 dr = 0.5\psi (R_o^4 - R_i^4) = 0.5m_{\text{cylinder}} (R_o^2 + R_i^2) \\ &= 0.5(0.8M)R^2(1 + 0.64) = 0.656MR^2 \end{aligned} \quad 0.5 \text{ pts}$$

$$\oint_{\text{rod}} r^2 dm = \mathbf{I} \int_0^{R_{in}} r^2 dr = \frac{1}{3} \mathbf{I} R_{in}^3 = \frac{1}{3} m_{\text{rod}} R_{in}^2 = \frac{1}{3} 0.025M (0.64R^2) = 0.00533MR^2 \quad 0.5 \text{ pts}$$

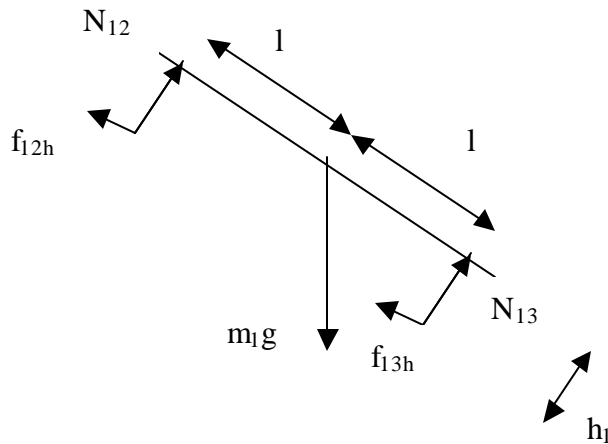
The moment inertia of each wheel becomes

$$I = 0.656MR^2 + 8 \times 0.00533MR^2 = 0.7MR^2 \quad 0.1 \text{ pts}$$

2. Force diagram and balance equations:

To simplify the analysis we divide the system into three parts: frame (part1) which mainly can be treated as flat homogeneous plate, rear cylinders (two cylinders are treated collectively as part 2 of the system), and front cylinders (two front cylinders are treated collectively as part 3 of the system).

Part 1 : Frame



0.4 pts

The balance equation related to the forces work to this parts are:

Required conditions:

Balance of force in the horizontal axis

$$m_1 g \sin \mathbf{q} - f_{12h} - f_{13h} = m_1 a \quad (1) \quad 0.2 \text{ pts}$$

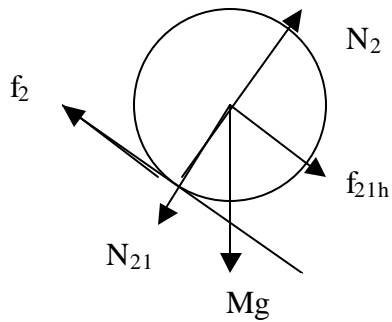
Balance of force in the vertical axis

$$m_1 g \cos \mathbf{q} = N_{12} + N_{13} \quad (2) \quad 0.2 \text{ pts}$$

Then torsi on against O is zero, so that

$$N_{12}l - N_{13}l + f_{12h}h_1 + f_{13h}h_1 = 0 \quad (3) \quad 0.2 \text{ pts}$$

Part two : Rear cylinder



0.25 pts

From balance condition in rear wheel :

$$f_{21h} - f_2 + Mg \sin \mathbf{q} = Ma \quad (4) \quad 0.15 \text{ pts}$$

$$N_2 - N_{21} - Mg \cos \mathbf{q} = 0 \quad (5) \quad 0.15 \text{ pts}$$

For pure rolling:

$$f_2 R = I \mathbf{a}_2 = I \frac{a_2}{R}$$

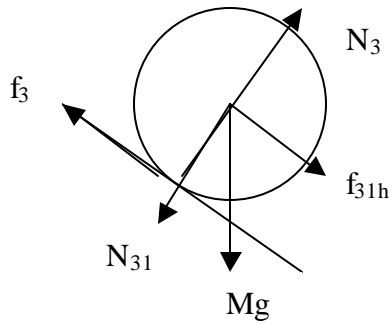
$$\text{or } f_2 = \frac{I}{R^2} a \quad (6)$$

For rolling with sliding:

$$F_2 = \mu_k N_2 \quad (7)$$

0.2 pts

Part Three : Front Cylinder:



0.25 pts

From balance condition in the front wheel 1 :

$$f_{31h} - f_3 + Mg \sin \theta = Ma \quad (8) \quad 0.15 \text{ pts}$$

$$N_3 - N_{31} - Mg \cos \theta = 0 \quad (9) \quad 0.15 \text{ pts}$$

For pure rolling:

$$f_3 R = I a_3 = I \frac{a_3}{R}$$

$$\text{or } f_3 = \frac{I}{R^2} a \quad (10)$$

For rolling with sliding:

$$F_3 = \mu_k N_3 \quad (11)$$

0.2 pts

3. From equation (2), (5) and (9) we get

$$\begin{aligned} m_1 g \cos \theta &= N_2 - m_2 g \cos \theta + N_3 - m_3 g \cos \theta \\ N_2 + N_3 &= (m_1 + m_2 + m_3) g \cos \theta = 7Mg \cos \theta \end{aligned} \quad (12)$$

And from equation (3), (5) and (8) we get

$$(N_3 - Mg \cos \theta) l - (N_2 - Mg \cos \theta) l = h_1 (f_2 + Ma - Mg \sin \theta + f_3 + Ma - Mg \sin \theta)$$

$$(N_3 - N_2) = h_1 (f_2 + 2Ma - 2Mg \sin \theta + f_3) / l$$

Equations 12 and 13 are given **0.25 pts**

CASE ALL CYLINDER IN PURE ROLLING

From equation (4) and (6) we get

$$f_{21h} = (I/R^2)a + Ma - Mg \sin\theta \quad (14) \quad 0.2 \text{ pts}$$

From equation (8) and (10) we get

$$f_{31h} = (I/R^2)a + Ma - Mg \sin\theta \quad (15) \quad 0.2 \text{ pts}$$

Then from eq. (1), (14) and (15) we get

$$5Mg \sin\theta - \{(I/R^2)a + Ma - Mg \sin\theta\} - \{(I/R^2)a + Ma - Mg \sin\theta\} = m_1 a$$

$$7 Mg \sin\theta = (2I/R^2 + 7M)a$$

$$a = \frac{7Mg \sin \mathbf{q}}{7M + 2\frac{I}{R^2}} = \frac{7Mg \sin \mathbf{q}}{7M + 2\frac{0.7MR^2}{R^2}} = 0.833g \sin \mathbf{q} \quad (16) \quad 0.35 \text{ pts}$$

$$\begin{aligned} N_3 &= \frac{7M}{2} g \cos \mathbf{q} + \frac{h_1}{l} [(M + \frac{I}{R^2}) \times 0.833g \sin \mathbf{q} - Mg \sin \mathbf{q}] \\ &= 3.5Mg \cos \mathbf{q} + \frac{h_1}{l} [(M + 0.7M) \times 0.833g \sin \mathbf{q} - Mg \sin \mathbf{q}] \\ &= 3.5 Mg \cos \mathbf{q} + 0.41 \frac{h_1}{l} Mg \sin \mathbf{q} \end{aligned}$$

$$\begin{aligned} N_2 &= \frac{7M}{2} g \cos \mathbf{q} - \frac{h_1}{l} [(\frac{I}{R^2} + M) \times 0.833g \sin \mathbf{q} - Mg \sin \mathbf{q}] \\ &= 3.5g \cos \mathbf{q} - \frac{h_1}{l} [(0.7M + M) \frac{7Mg \sin \mathbf{q}}{0.7M + 7M} - 2Mg \sin \mathbf{q}] \\ &= 3.5g \cos \mathbf{q} - 0.41 \frac{h_1}{l} Mg \sin \mathbf{q} \end{aligned}$$

0.2 pts

The Conditions for pure rolling:

$$f_2 \leq \mathbf{m}_s N_2 \quad \text{and} \quad f_3 \leq \mathbf{m}_s N_3$$

$$\frac{I_2}{R_2^2} a \leq \mathbf{m}_s N_2 \quad \text{and} \quad \frac{I_3}{R_3^2} a \leq \mathbf{m}_s N_3$$

0.2 pts

The left equation becomes

$$0.7M \times 0.833g \sin \mathbf{q} \leq \mathbf{m}_s (3.5Mg \cos \mathbf{q} - 0.41 \frac{h_1}{l} Mg \sin \mathbf{q})$$

$$\tan \mathbf{q} \leq \frac{3.5\mathbf{m}_s}{0.5831 + 0.41\mathbf{m}_s \frac{h_1}{l}}$$

While the right equation becomes

$$0.7m \times 0.833g \sin \mathbf{q} \leq \mathbf{m}_s (3.5mg \cos \mathbf{q} + 0.41 \frac{h_1}{l} mg \sin \mathbf{q})$$

$$\tan \mathbf{q} \leq \frac{3.5\mathbf{m}_s}{0.5831 - 0.41\mathbf{m}_s \frac{h_1}{l}}$$

(17) 0.1 pts

CASE ALL CYLINDER SLIDING

$$\text{From eq. (4)} \quad f_{21h} = Ma + u_k N_2 - Mg \sin \theta \quad (18) \quad 0.15 \text{ pts}$$

$$\text{From eq. (8)} \quad f_{31h} = Ma + u_k N_3 - Mg \sin \theta \quad (19) \quad 0.15 \text{ pts}$$

From eq. (18) and 19 :

$$5Mg \sin \theta - (Ma + u_k N_2 - Mg \sin \theta) - (Ma + u_k N_3 - Mg \sin \theta) = m_1 a$$

$$a = \frac{7Mg \sin \mathbf{q} - \mathbf{m}_k N_2 - \mathbf{m}_k N_3}{7M} = g \sin \mathbf{q} - \frac{\mathbf{m}_k (N_2 + N_3)}{7M} \quad (20) \quad 0.2 \text{ pts}$$

$$N_3 + N_2 = 7Mg \cos \mathbf{q}$$

From the above two equations we get :

$$a = g \sin \mathbf{q} - \mathbf{m}_k g \cos \mathbf{q} \quad 0.25 \text{ pts}$$

The Conditions for complete sliding: are the opposite of that of pure rolling

$$\begin{aligned} f_2 > \mathbf{m}_s N'_2 & \quad \text{and} \quad f_3 > \mathbf{m}_s N'_3 \\ \frac{I_2}{R_2^2} a > \mathbf{m}_s N'_2 & \quad \text{and} \quad \frac{I_3}{R_3^2} a > \mathbf{m}_s N'_3 \end{aligned} \quad (21) \quad 0.2 \text{ pts}$$

Where N_2' and N_3' is calculated in case all cylinder in pure rolling. 0.1 pts

Finally we get

$$\tan \mathbf{q} > \frac{3.5\mathbf{m}_s}{0.5831 + 0.41\mathbf{m}_s \frac{h_1}{l}} \quad \text{and} \quad \tan \mathbf{q} > \frac{3.5\mathbf{m}_s}{0.5831 - 0.41\mathbf{m}_s \frac{h_1}{l}} \quad 0.2 \text{ pts}$$

The left inequality finally become decisive.

CASE ONE CYLINDER IN PURE ROLLING AND ANOTHER IN SLIDING CONDITION

{ For example R_3 (front cylinders) pure rolling while R_2 (Rear cylinders) sliding }

From equation (4) we get

$$F_{21h} = m_2 a + \mu_k N_2 - m_2 g \sin \theta \quad (22) \quad 0.15 \text{ pts}$$

From equation (5) we get

$$f_{31h} = m_3 a + (I/R^2) a - m_3 g \sin \theta \quad (23) \quad 0.15 \text{ pts}$$

Then from eq. (1), (22) and (23) we get

$$m_1 g \sin \theta - \{ m_2 a + \mu_k N_2 - m_2 g \sin \theta \} - \{ m_3 a + (I/R^2) a - m_3 g \sin \theta \} = m_1 a$$

$$m_1 g \sin \theta + m_2 g \sin \theta + m_3 g \sin \theta - \mu_k N_2 = (I/R^2 + m_3) a + m_2 a + m_1 a$$

$$5Mg \sin \theta + Mg \sin \theta + Mg \sin \theta - \mu_k N_2 = (0.7M + M) a + Ma + 5Ma$$

$$a = \frac{7Mg \sin \theta - \mu_k N_2}{7.7M} = 0.9091g \sin \theta - \frac{\mu_k N_2}{7.7M} \quad (24) \quad 0.2 \text{ pts}$$

$$N_3 - N_2 = \frac{h_1}{l} (\mu_k N_2 + \frac{I}{R^2} a + 2Ma - 2Mg \sin \theta)$$

$$N_3 - N_2 = \frac{h_1}{l} (\mu_k N_2 + 2.7M \times 0.9091g \sin \theta - 2.7 \mu_k N_2 / 7.7 - 2Mg \sin \theta)$$

$$N_3 - N_2 (1 + 0.65 \mu_k \frac{h_1}{l}) = 0.4546Mg \sin \theta$$

$$N_3 + N_2 = 7Mg \cos \theta$$

Therefore we get

$$N_2 = \frac{7Mg \cos \theta - 0.4546Mg \sin \theta}{2 + 0.65 \mu_k \frac{h_1}{l}} \quad (25) \quad 0.3 \text{ pts}$$

$$N_3 = 7Mg \cos \theta - \frac{7Mg \cos \theta - 0.4546Mg \sin \theta}{2 + 0.65 \mu_k \frac{h_1}{l}}$$

Then we can substitute the results above into equation (16) to get the following result

$$a = 0.9091g \sin \theta - \frac{\mu_k N_2}{7.7M} = 0.9091g \sin \theta - \frac{\mu_k}{7.7} \frac{7g \cos \theta - 0.4546g \sin \theta}{2 + 0.65 \mu_k \frac{h_1}{l}} \quad (26)$$

0.2 pts

The Conditions for this partial sliding is:

$$f_2 \leq \mu_3 N'_2 \quad \text{and} \quad f_3 > \mu_3 N'_3$$

$$\frac{I}{R^2} a \leq \mu_3 N'_2 \quad \text{and} \quad \frac{I}{R^2} a > \mu_3 N'_3 \quad (27) \quad 0.25 \text{ pts}$$

where N'_2 and N'_3 are normal forces for pure rolling condition

4. Assumed that after rolling d meter all cylinder start to sliding until reaching the end of incline road (total distant is s meter). Assumed that t_1 meter is reached in t_1 second.

$$v_{t1} = v_o + at_1 = 0 + a_1 t_1 = a_1 t_1$$

$$d = v_o t_1 + \frac{1}{2} a_1 t_1^2 = \frac{1}{2} a_1 t_1^2$$

$$t_1 = \sqrt{\frac{2d}{a_1}}$$

0.5 pts

$$v_{t1} = a_1 \sqrt{\frac{2d}{a_1}} = \sqrt{2da_1} = \sqrt{2d \cdot 0.833g \sin \mathbf{q}} = \sqrt{1.666dg \sin \mathbf{q}} \quad (28)$$

The angular velocity after rolling d meters is same for front and rear cylinders:

$$\mathbf{w}_{t1} = \frac{v_{t1}}{R} = \frac{1}{R} \sqrt{1.666dg \sin \mathbf{q}} \quad (29)$$

0.5 pts

Then the vehicle sliding until the end of declining road. Assumed that the time needed by vehicle to move from d position to the end of the declining road is t_2 second.

$$v_{t2} = v_{t1} + a_2 t_2 = \sqrt{1.666dg \sin \mathbf{q}} + a_2 t_2$$

$$s - d = v_{t1} t_2 + \frac{1}{2} a_2 t_2^2$$

$$t_2 = \frac{-v_{t1} + \sqrt{v_{t1}^2 + 2a_2(s-d)}}{a_2} \quad (30) \quad 0.4 \text{ pts}$$

$$v_{t2} = \sqrt{1.666dg \sin \mathbf{q}} - v_{t1} + \sqrt{v_{t1}^2 + 2a_2(s-d)}$$

Inserting v_{t1} and a_2 from the previous results we get the final results.

For the angular velocity, while sliding they receive torsion:

$$t = m_k NR$$

$$\mathbf{a} = \frac{t}{I} = \frac{m_k NR}{I} \quad (31)$$

$$w_{t2} = w_{t1} + \mathbf{a}t_2 = \frac{1}{R} \sqrt{1.666 dg \sin \mathbf{q}} + \frac{m_k NR}{I} \frac{-v_{t1} + \sqrt{v_{t1}^2 + 2a_2(s-d)}}{a_2}$$

0.6 pts